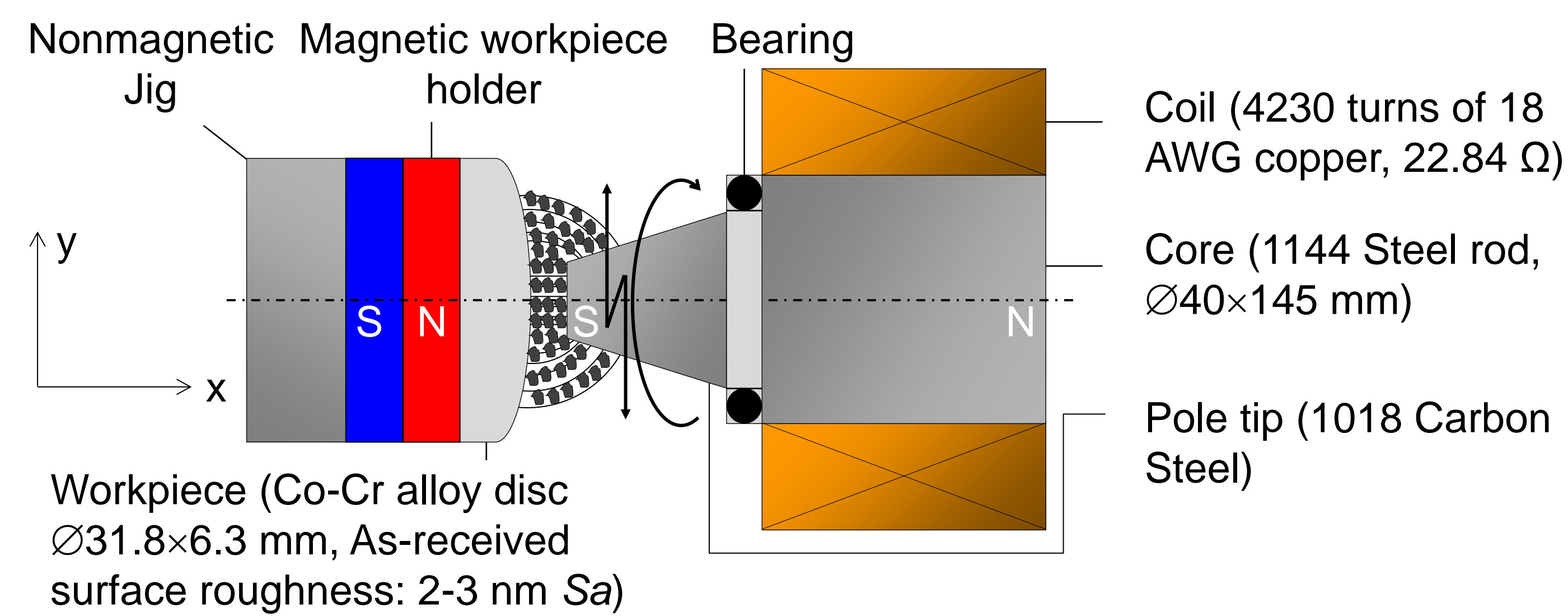


CHARACTERISTICS OF COBALT CHROMIUM ALLOY SURFACES FINISHED USING MAGNETIC ABRASIVE FINISHING

MAGNETIC ABRASIVE FINISHING



Schematic of Processing Principle

Magnetic abrasive particles are linked by magnetic force, F , in a magnetic field

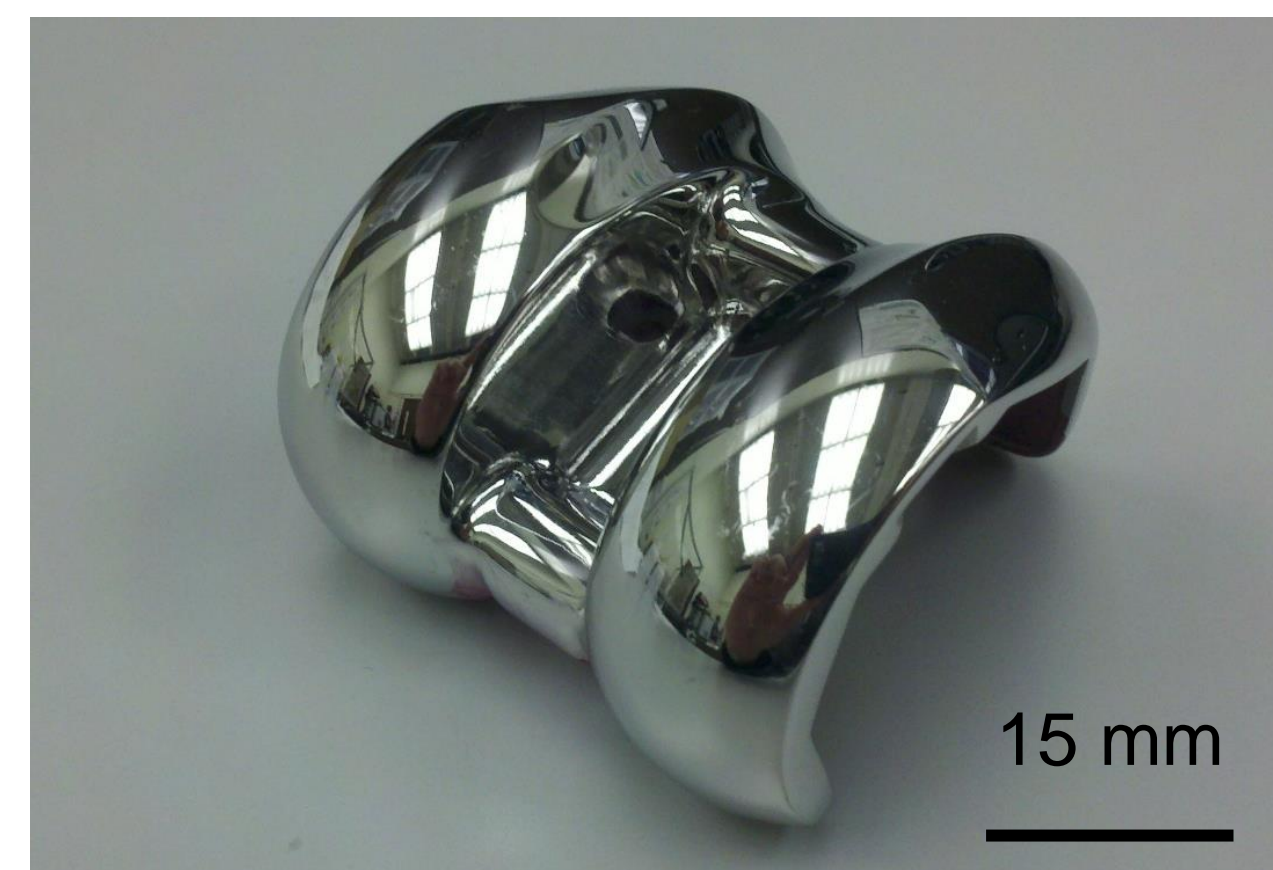
$$F = V\chi \cdot H \cdot \nabla H$$

V : Volume of magnetic particle

χ : Magnetic susceptibility

$H, \nabla H$: Magnetic field intensity and its gradient

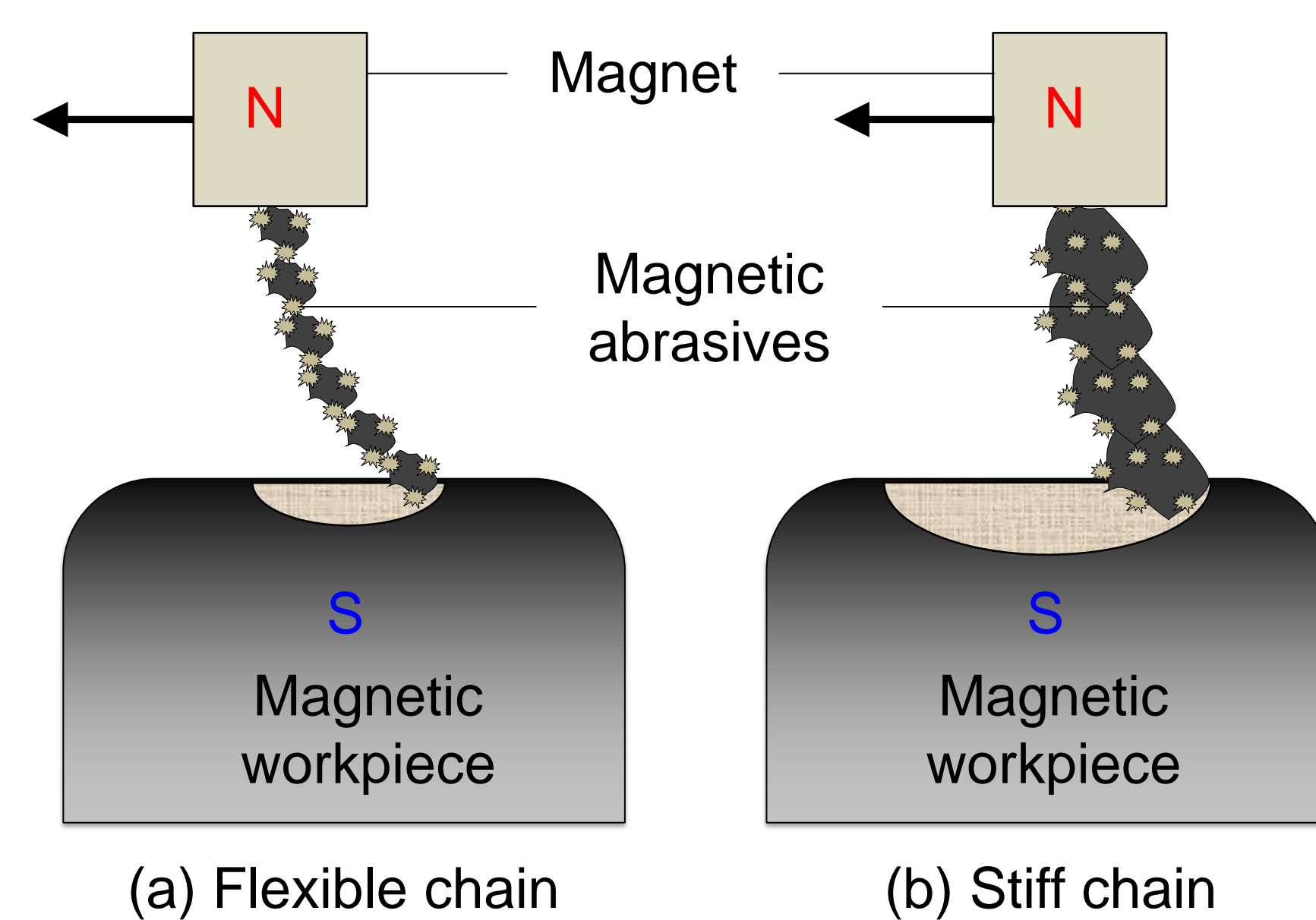
When the pole tip rotates, the magnetic abrasives rotate with the pole tip. This generates relative motion against the target surface and finishes it smoothly. The feed motion of the workpiece (attached to a robot) extends the finishing area in the y direction.



Femoral Knee Component

FINISHING CONDITIONS

Increasing the magnetic field intensity or magnetic abrasive size increases the particle chain stiffness, resulting in longer cutting marks. Four finishing conditions were developed to generate four kinds of surface lays on a flat Co-Cr alloy workpiece.



Schematic of Magnetic Brush

Arthur Graziano¹, Vasishta Ganguly²,
Tony Schmitz², and Hitomi Yamaguchi¹
¹University of Florida, Gainesville, FL
²University of North Carolina at Charlotte, Charlotte NC

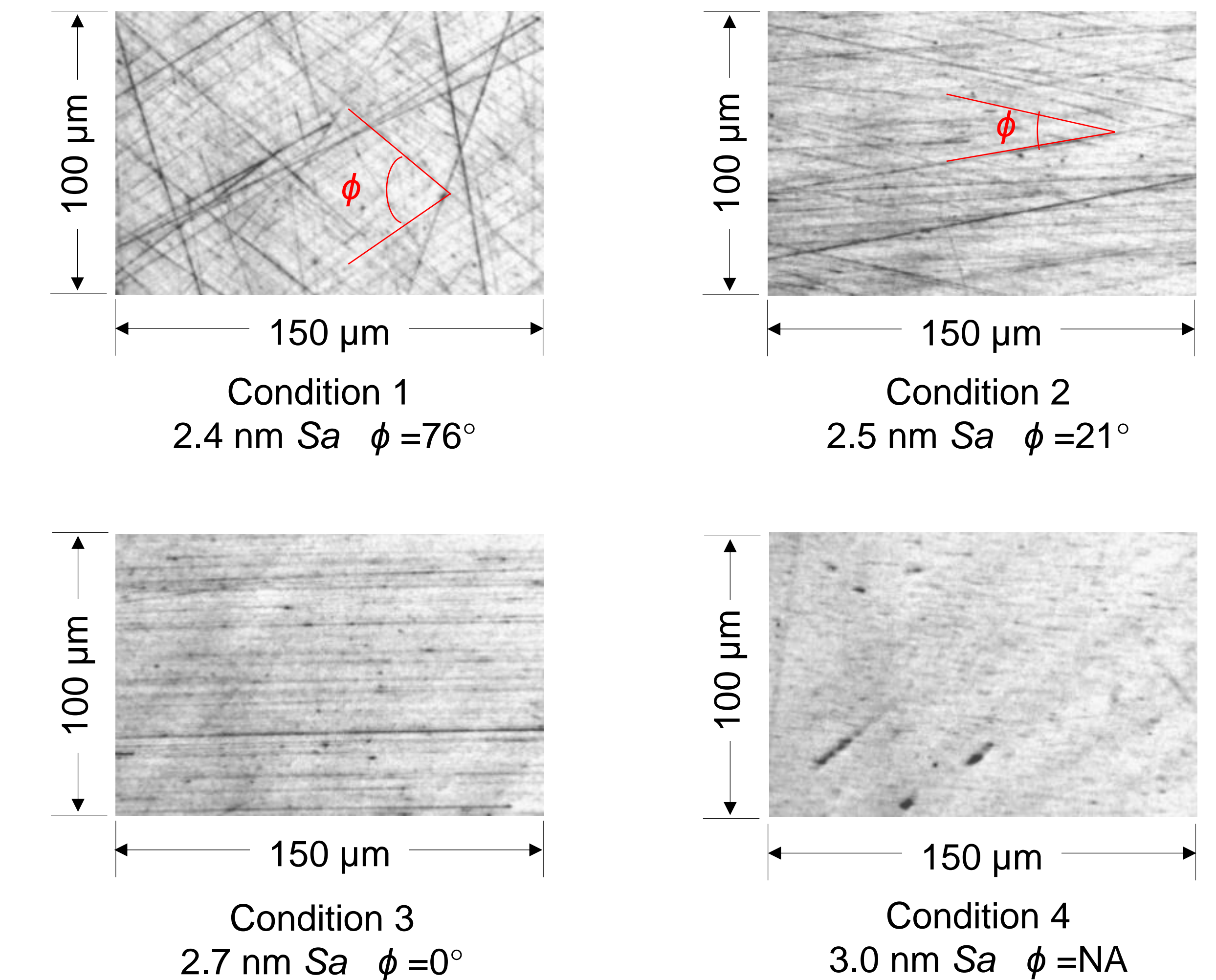
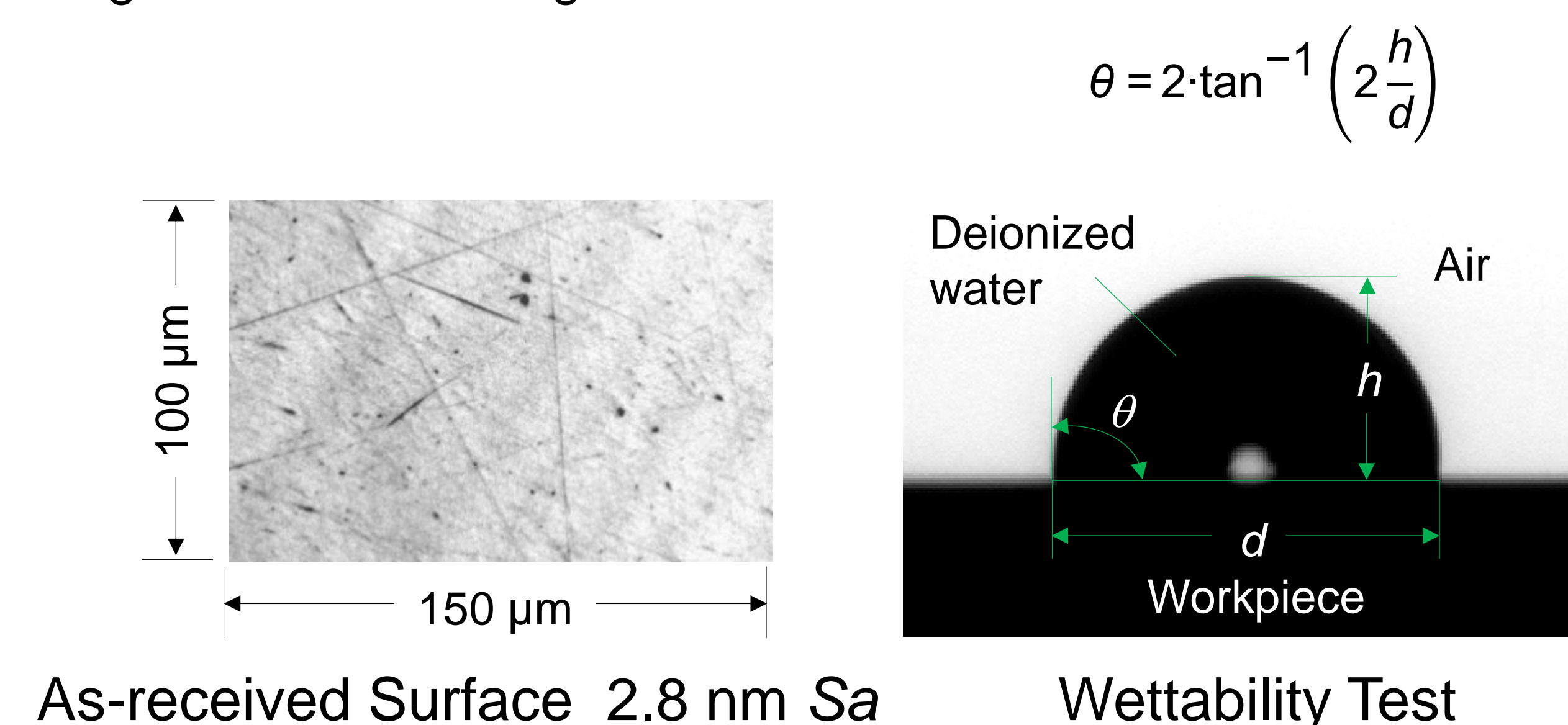
FREEFORM SURFACES, INCLUDING THE FEMORAL COMPONENT OF KNEE PROSTHETICS, PRESENT A SIGNIFICANT CHALLENGE IN MANUFACTURING. SURFACE FINISH VARIATIONS CAN LEAD TO ACCELERATED WEAR OF THE ULTRA HIGH MOLECULAR WEIGHT POLYETHYLENE (UHMWPE) TIBIAL COMPONENT. THIS STUDY APPLIES MAGNETIC ABRASIVE FINISHING (MAF) FOR NANOMETER-SCALE FINISHING OF COBALT CHROMIUM ALLOYS, WHICH ARE COMMONLY USED IN KNEE PROSTHETICS. THE GOAL OF THIS STUDY IS TO DEMONSTRATE THE FEASIBILITY OF MAF TO ALTER THE LAY, WHILE CONTROLLING THE SURFACE ROUGHNESS. THE EFFECTS OF LAY ON WETTABILITY AND COEFFICIENT OF FRICTION ARE ALSO STUDIED.

Finishing Conditions

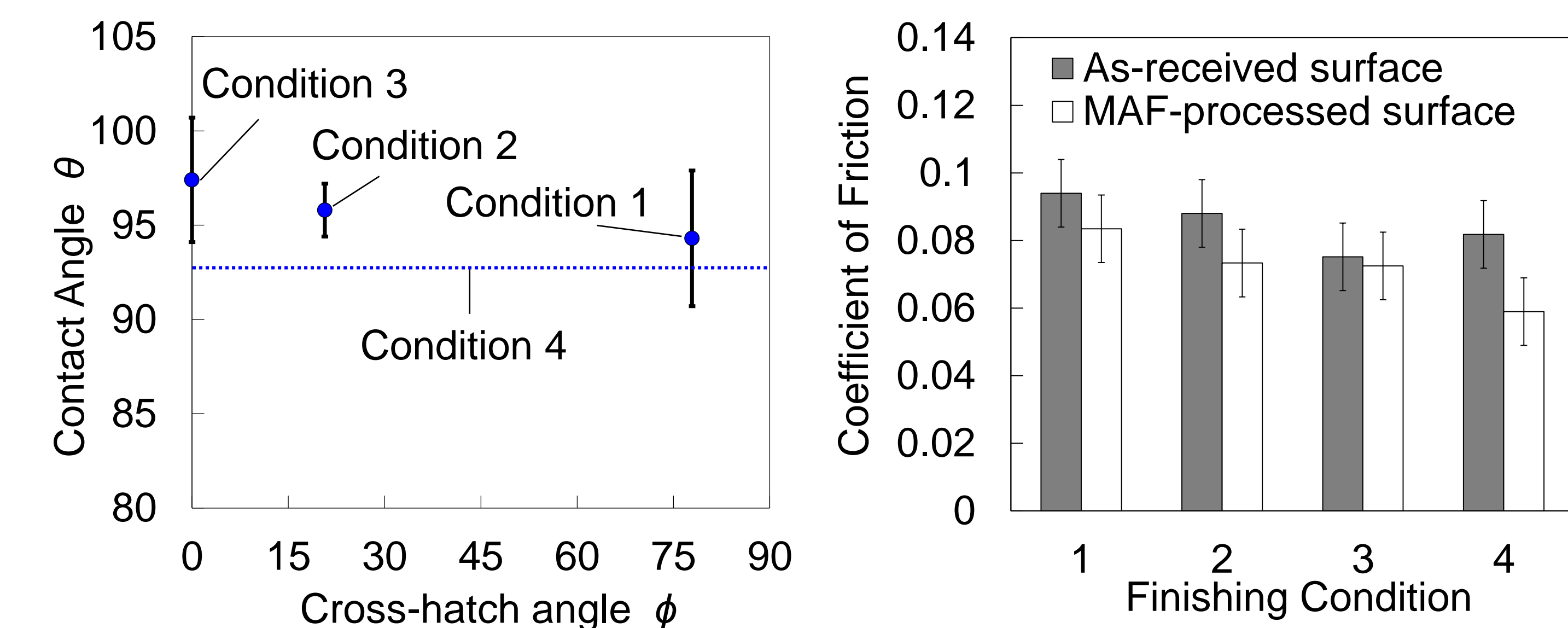
| Condition | 1 | 2 | 3 | 4 | |
|--|--------|--------|--------|--------|------|
| Diamond abrasive size, μm | 0-0.25 | 0-0.25 | 0-0.5 | 0-0.25 | |
| Diamond abrasive amount, mg | 50 | 50 | 50 | 50 | |
| Iron particle size, μm | 45-150 | 45-150 | 45-150 | 0-45 | |
| Iron particle amount, mg | 500 | 500 | 500 | 500 | 300 |
| Workpiece feed rate, mm/s | 50 | 10 | 1 | 1 | |
| Workpiece feed, mm | 43 | 43 | 43 | 43 | |
| Pole tip revolution, min^{-1} | 100 | 100 | 500 | 500 | 150 |
| Clearance between pole tip and workpiece, mm | 1 | 1 | 1 | 1 | |
| Magnetic flux density (1mm from pole tip), T | 0.23 | 0.23 | 0.23 | 0.23 | 0.13 |
| Finishing time, min | 15 | 15 | 15 | 15 | 45 |

SURFACE CHARACTERIZATION

The relationship between the surface lay, contact angle (measure of wettability) and coefficient of friction of nanometer-scale surface roughness was investigated.



Images of MAF-finished Surfaces Captured by an Optical Profilometer



CONCLUSIONS

1. Finishing experiments on flat workpieces demonstrated the feasibility of MAF to alter surface lay while controlling the nanometer-scale surface roughness by changing the length, depth, and direction of cutting marks.
2. Surfaces with unidirectional cutting marks exhibit the least wettability, and increasing the cross-hatch angle in the MAF-produced surfaces increases the wettability.
3. Surfaces consisting of short, intermittent cutting marks with less directionality are the most wettable.
4. MAF-processed surfaces show a decrease in coefficient of friction due to their reduced surface roughness.

ACKNOWLEDGEMENTS: This work was supported by the National Science Foundation (Grant No. CMMI-0855381). The authors gratefully acknowledge the 2012 American Society of Mechanical Engineers Elisabeth M. and Winchell M. Parsons Scholarship. The authors also would like to thank James C. Wilkes, J. Whittaker Bullard, and Matt Moore for their interest in this work and Exactech, Inc. for their support in the workpiece preparation.